

# Thermal Modeling of the Solar Corona

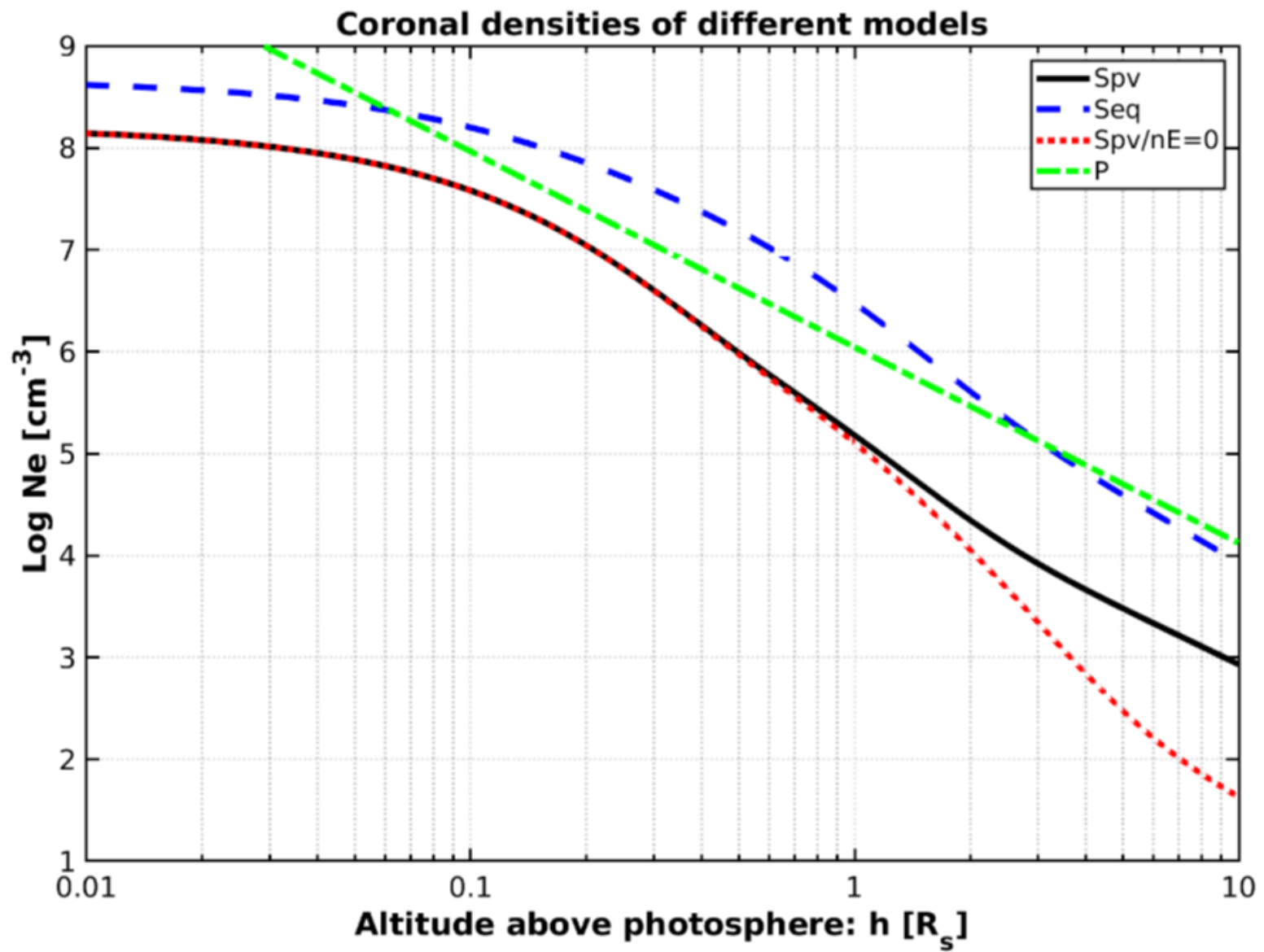
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# Layout of the talk

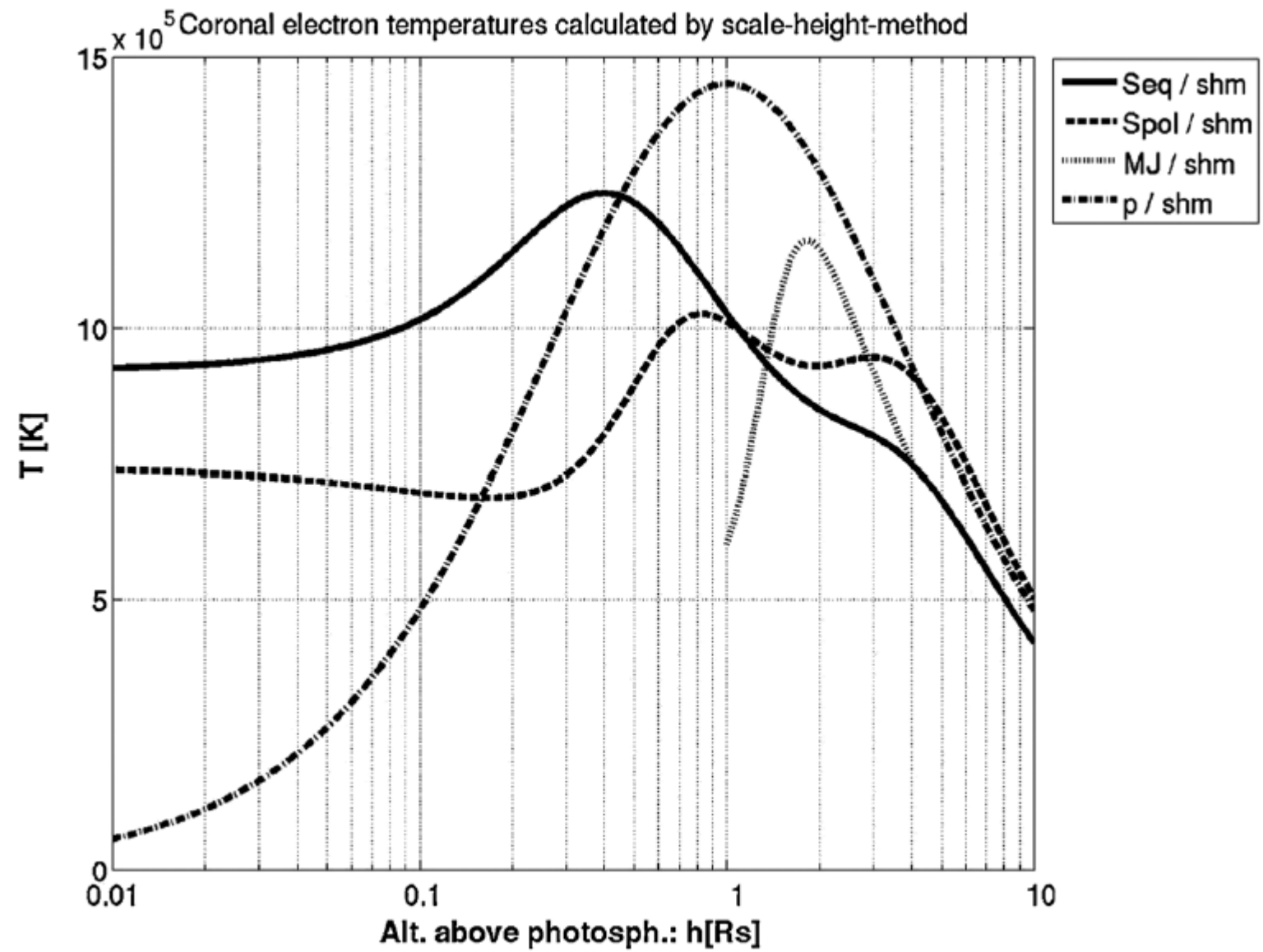
- Existing models of the ambient corona and their limitations
- The temperature profiles derived by the models

# The Scale-Height model

- $H = K * T / \mu * m_H * g = - [d(\ln n_e) / dr]^{-1}$
- 1<sup>st</sup> problem:  $g = g(r) = g_0 * R_S^2 / r^2$  (Chapman 1957)
- 2<sup>nd</sup> problem:  $H$  not constant, i.e. corona not isothermal
- $H$  not quasi-isothermal either (i.e.  $d(\ln n_e) / dr$  not approximately exponential). Saito (1970)'s fit doesn't satisfy  $p_e \approx n_e * k * T$



Lemaire and Katsiyannis (2021)



Lemaire and Stegen (2016)

# The HST model

- Adds the  $dT/dr$  factor:

$$dT(r)/dr + [d(\ln n_e)/dr]^{-1} = - \mu^* m_H^* g^* R_S^2 / (k r^2)$$

- Alfvén (1941) had already solved equations numerically.
- Problem: No solar wind!!

# Parker's model

- Adds the  $\rho \, du/dt$  factor:

$$dT(r)/dr + [d(\ln n_e)/dr]^{-1} + \mu^* m_H^* g^* R_S^2 / (k \, r^2) + \rho \, du/dt = 0,$$

where  $\rho = m_H n_e(r)$  and  $n_e(r)$  decreases exponentially.

- 1<sup>st</sup> problem: Needs precise assumptions for the boundary condition of  $u_0$  so  $u(r)$  is continuous and passes through a saddle point at the distance where the bulk speed becomes supersonic (Parker 1963).
- 2<sup>nd</sup> problem: It only diverges for  $T(\infty)=0$ . Pottach (1960), Brandt et al (1965), and Gibson et al (1999) used  $T(\infty)=0$  and  $P(\infty)=0$ . Even slightly different boundary conditions will produce diverging steady state solutions.

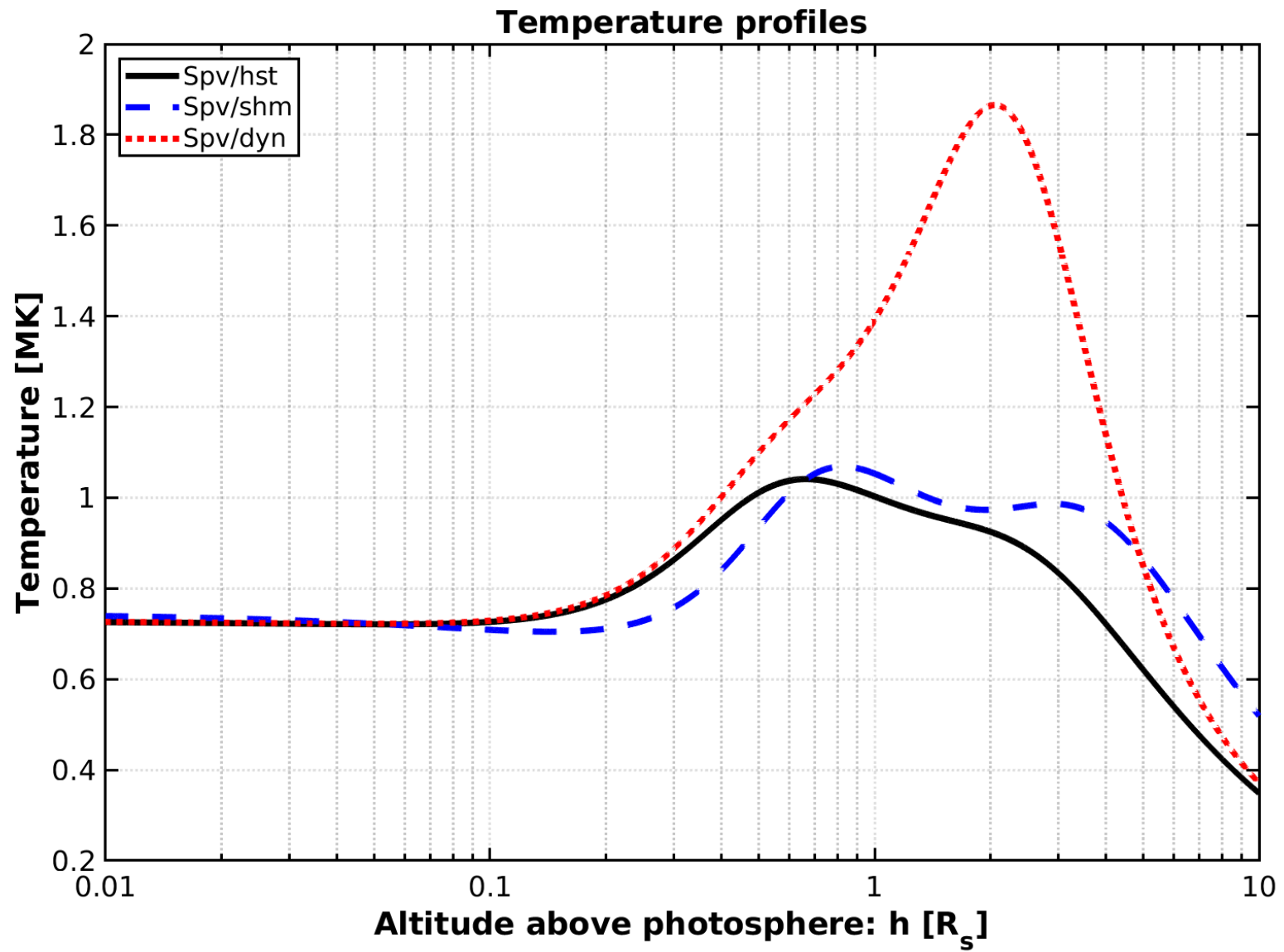
# The DYN model

- Lemaire & Stegen (2016) also added a term to Saito (1970)'s fit. This was to correct for  $n_e(1\text{AU})$ . Saito (1970)'s fit up to  $4 R_s$ :

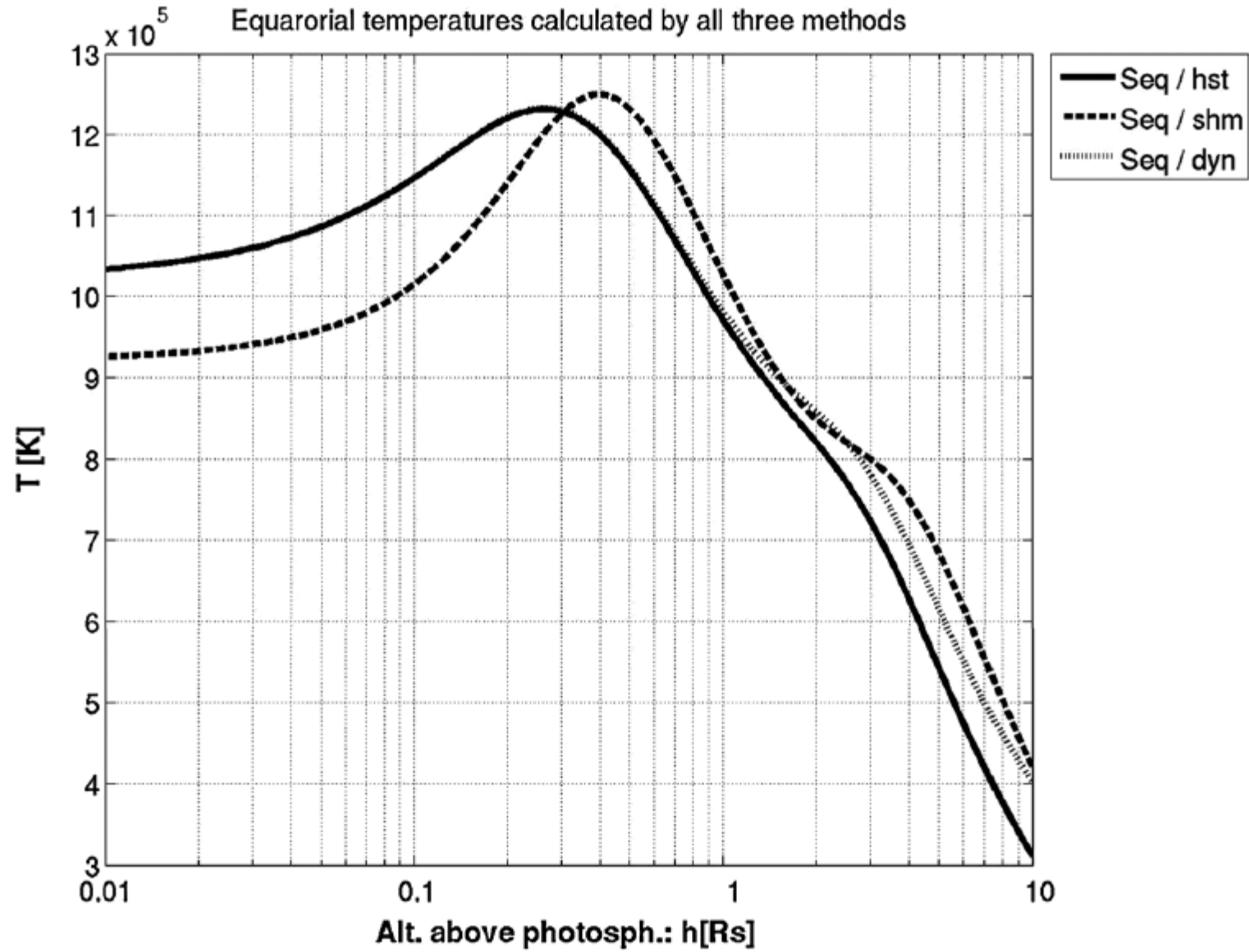
$$n_e(r) = 10^8 [3.09 r^{-16} (1 - 0.5 \sin(\varphi)) + 1.58 r^{-6} (1 - 0.95 \sin(\varphi)) + 0.0251 r^{-2.5} (1 - \sqrt{\sin(\varphi)})] + n_e(1\text{AU}) (215/r)^2$$

- Boundary conditions ( $n_E$  and  $u_E$ ) are set at 1 AU.
- $u(r, \varphi) = u_E A_E / A(r) n_E / n_e(r, \varphi)$ ,  
where  $A$  is the cross section of the flow tubes.

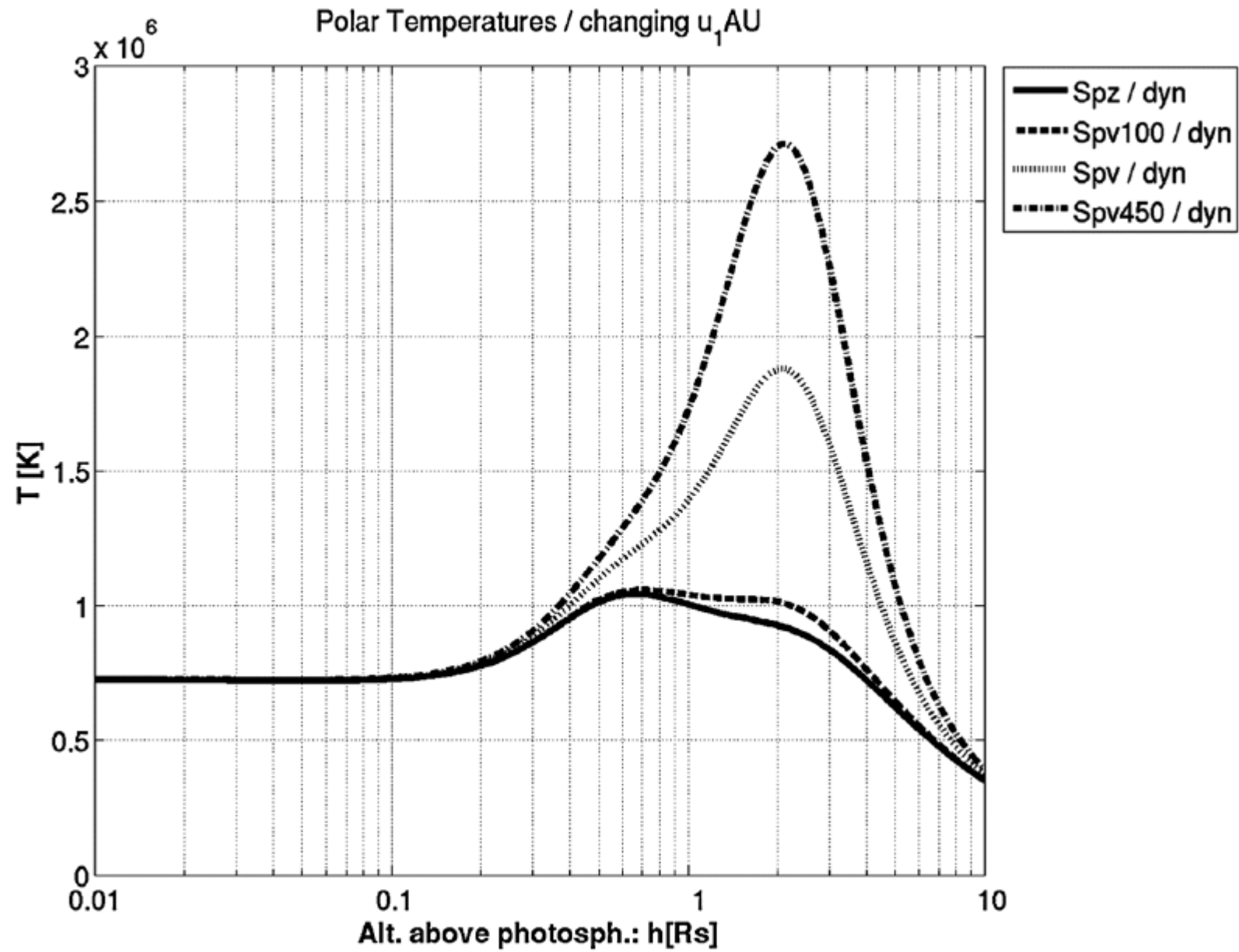




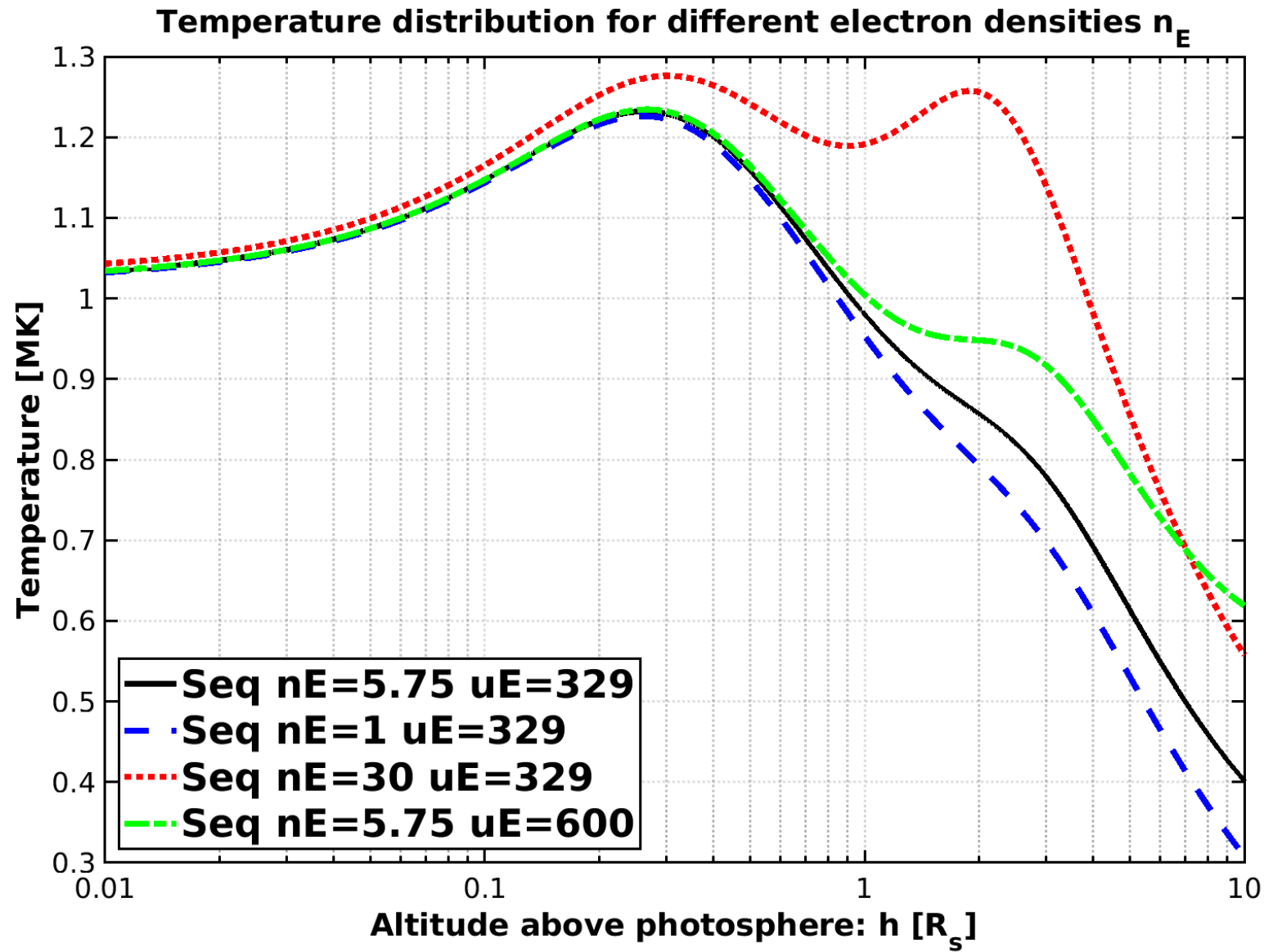
Lemaire and Katsiyannis (2021)



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